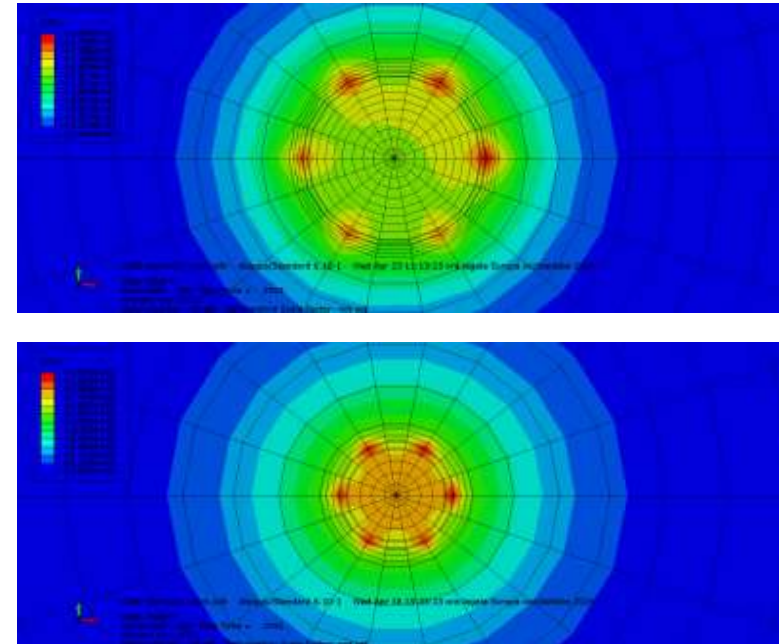
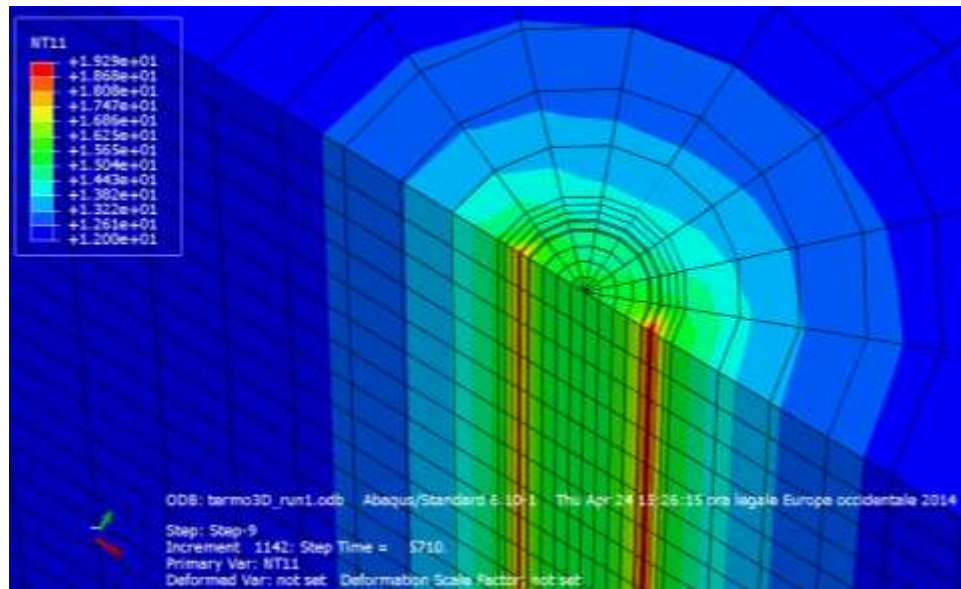


A new modelling approach for piled and other ground heat exchanger applications



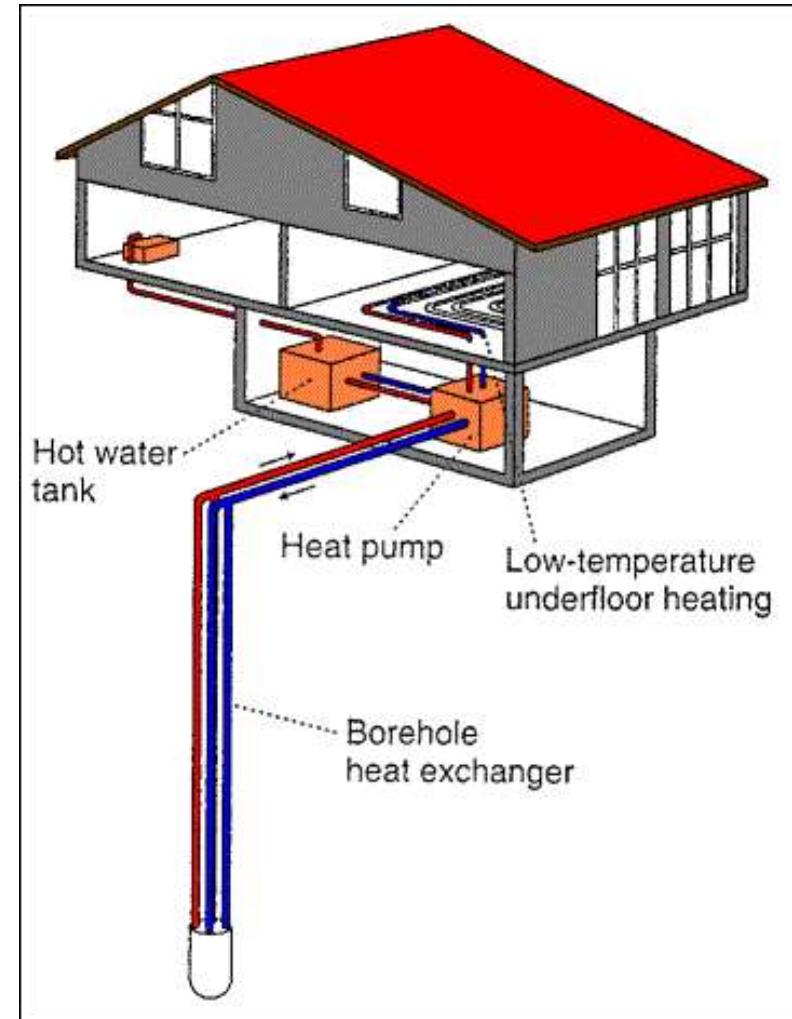
F. Cecinato¹, F. Loveridge²

¹Department of Civil, Environmental and Mechanical Engineering, University of Trento, Italy

²Faculty of Civil Engineering & Environment, University of Southampton, UK

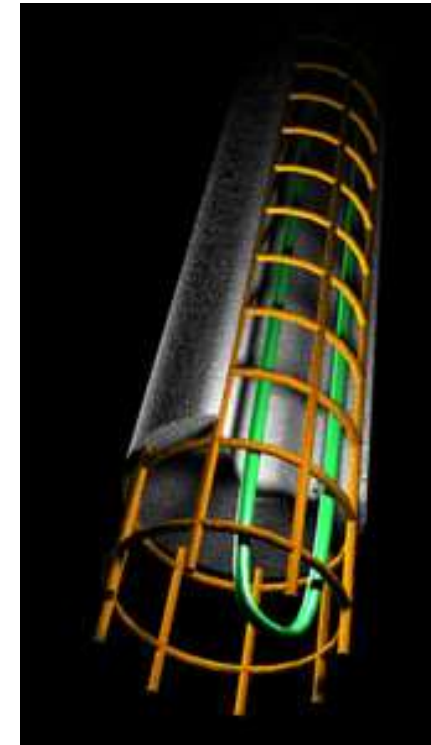
Ground heat exchangers

- **Borehole heat exchanger (BHE):** heat exchanger installed inside a borehole ($\varnothing=10\text{-}20\text{ cm}$)
- routinely designed with commercial software
- with a simplified approach (linear infinite heat source, steady-state assumptions)

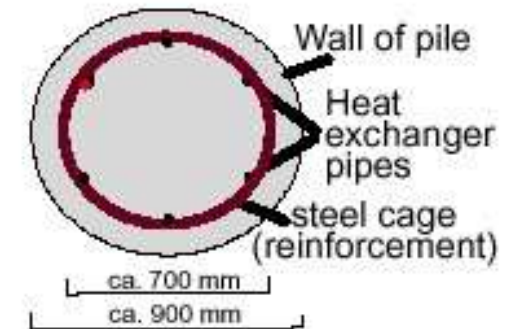


Ground heat exchangers

- **Energy pile (EP):** heat exchanger installed inside a piled foundation ($\varnothing = 0.3\text{-}2.0\text{ m}$)
- routinely designed with 'mechanical criteria'. BHEs' Simplified thermal analysis is not adequate, since:
 - Different aspect ratio compared to BHEs
 - > the linear infinite source approximation doesn't apply
 - Much larger diameter
 - > important transient heat transfer effects



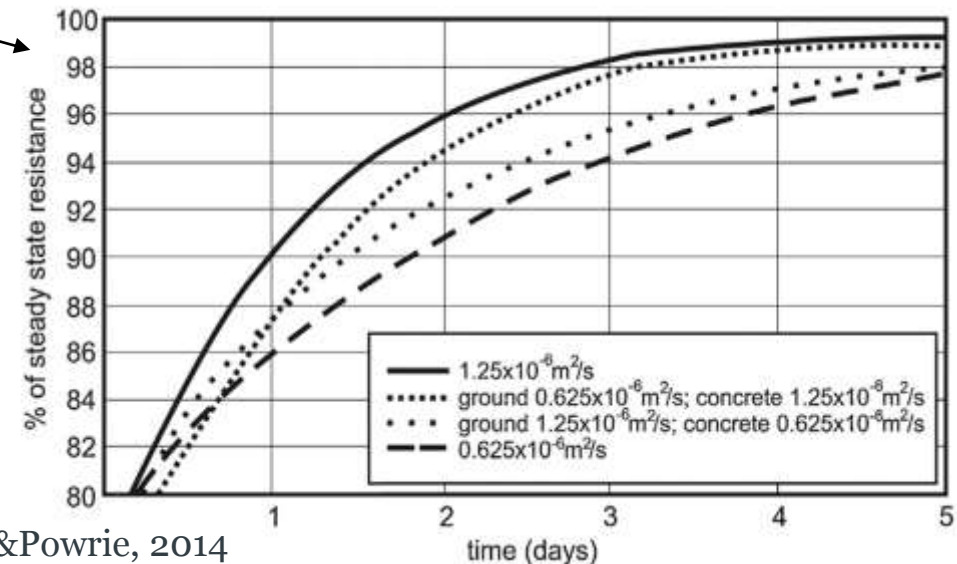
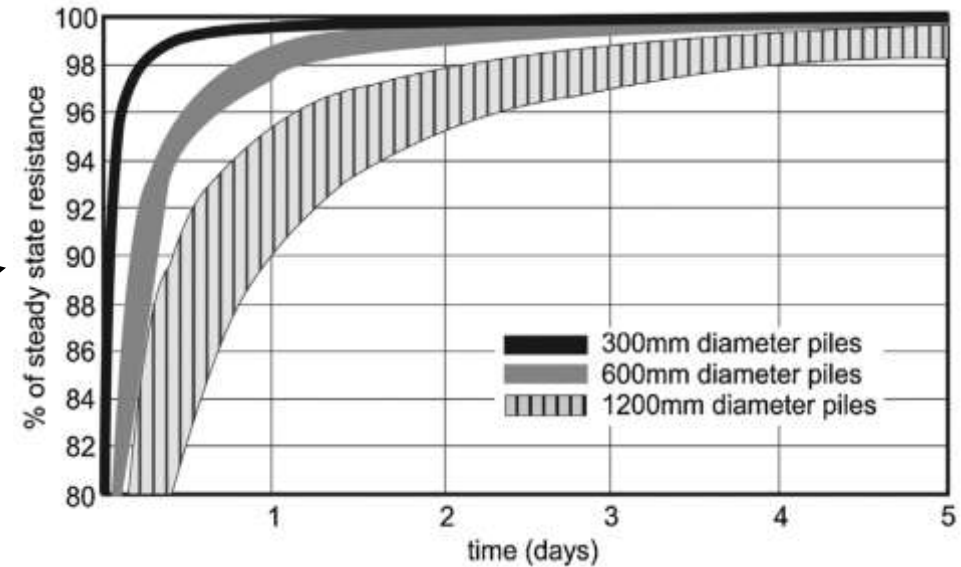
<http://www.geothermie.de/>



<http://www.geothermie.de/>

Actual thermal behaviour of EPs

- The time needed to reach steady state depends on
 - \varnothing pile, no. & position of pipes, thermal conductivity
 - Type of heat pulse
- Surface temperature changes both along a vertical and horizontal section: 3D effects



FEM numerical model

Use of software ABAQUS

- To integrate 3D transient conduction through the concrete & the ground

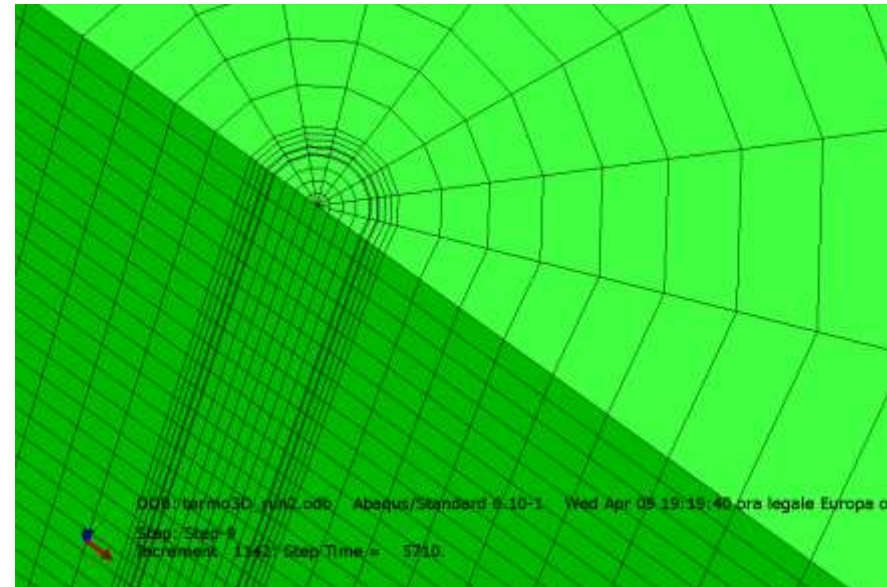
$$\rho_s c_{ps} \dot{T} = \nabla (\lambda_s \nabla T)$$

+ Bespoke user subroutines

- To model the convective heat transfer at the fluid/solid interface and the temperature changes in the fluid along the pipe

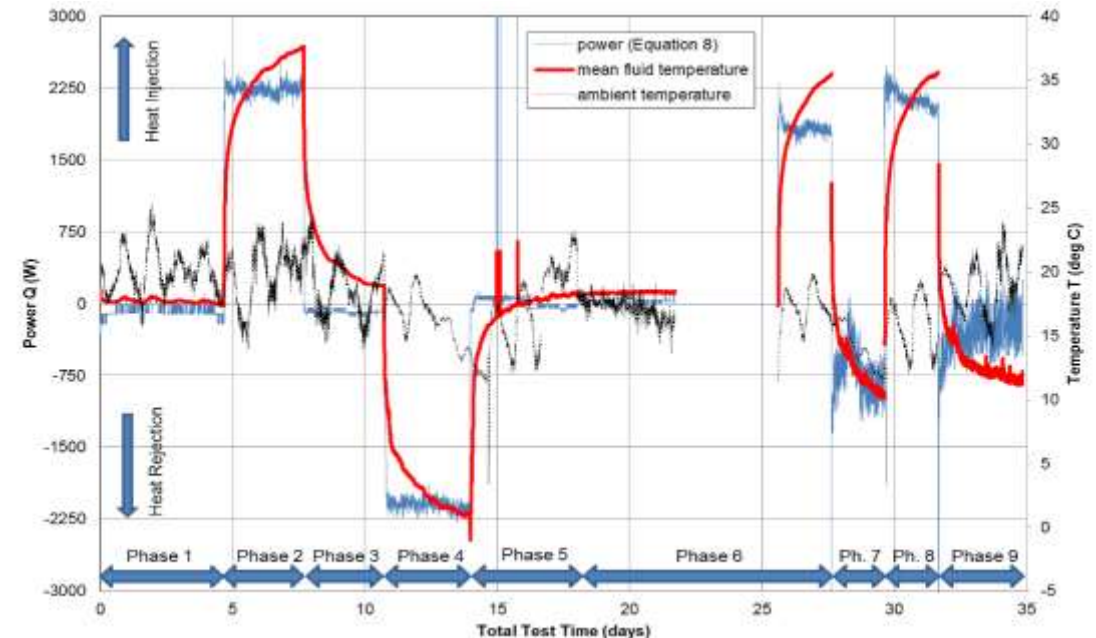
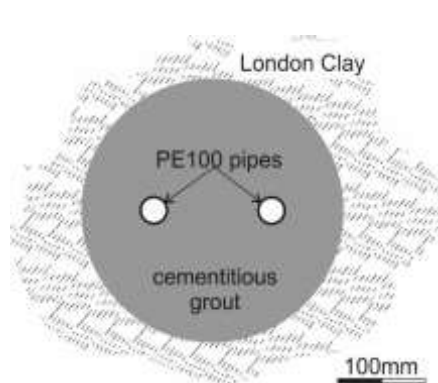
$$\dot{m} c_{pf} \nabla T = h \Delta T$$

- 3D FE mesh manually created to minimise computational time
- Symmetry can be exploited for single U-pipe EPs



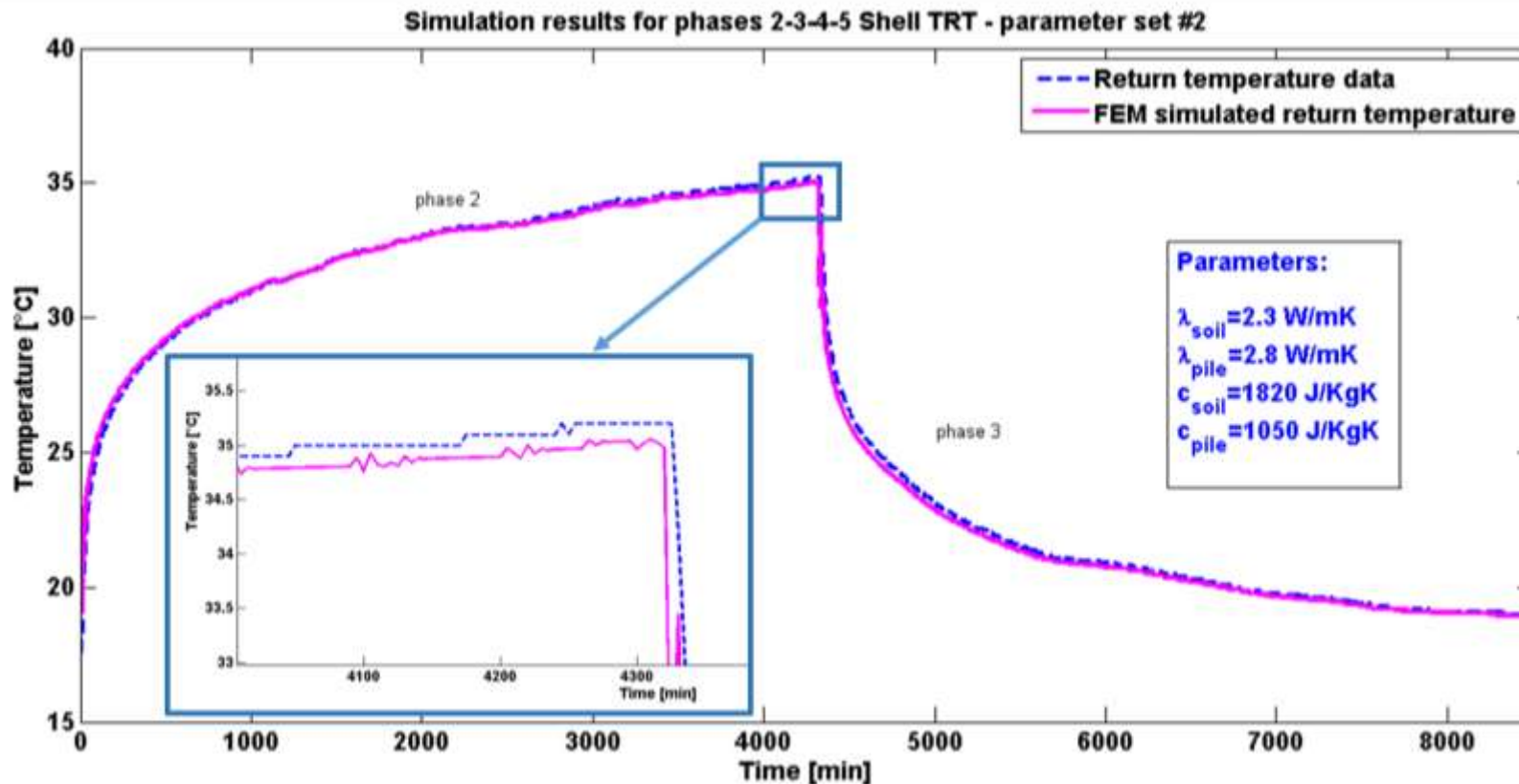
Numerical model validation against field data

- The outcome of a thermal response test (TRT) on a single test pile installed in London clay was reproduced
 - $\varnothing=30$ cm, $L=27$ m, single U-pipe, equipped with sensors measuring both concrete and exchanger fluid temperature
- Input data:
 - * Inlet fluid temperature
 - * Geometry & thermal properties of materials



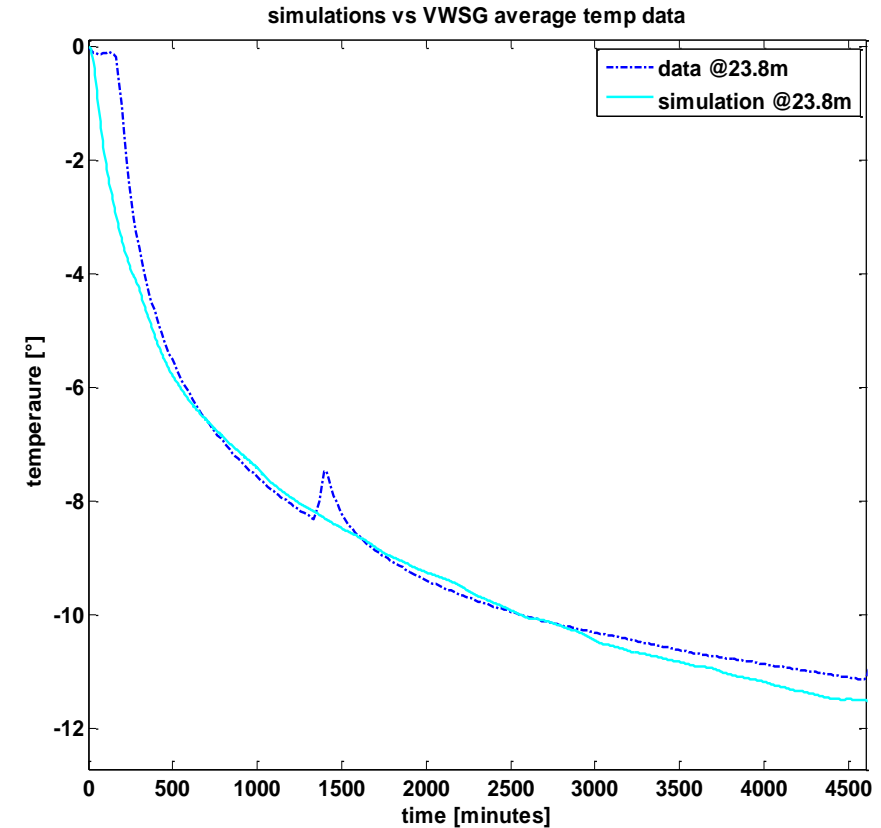
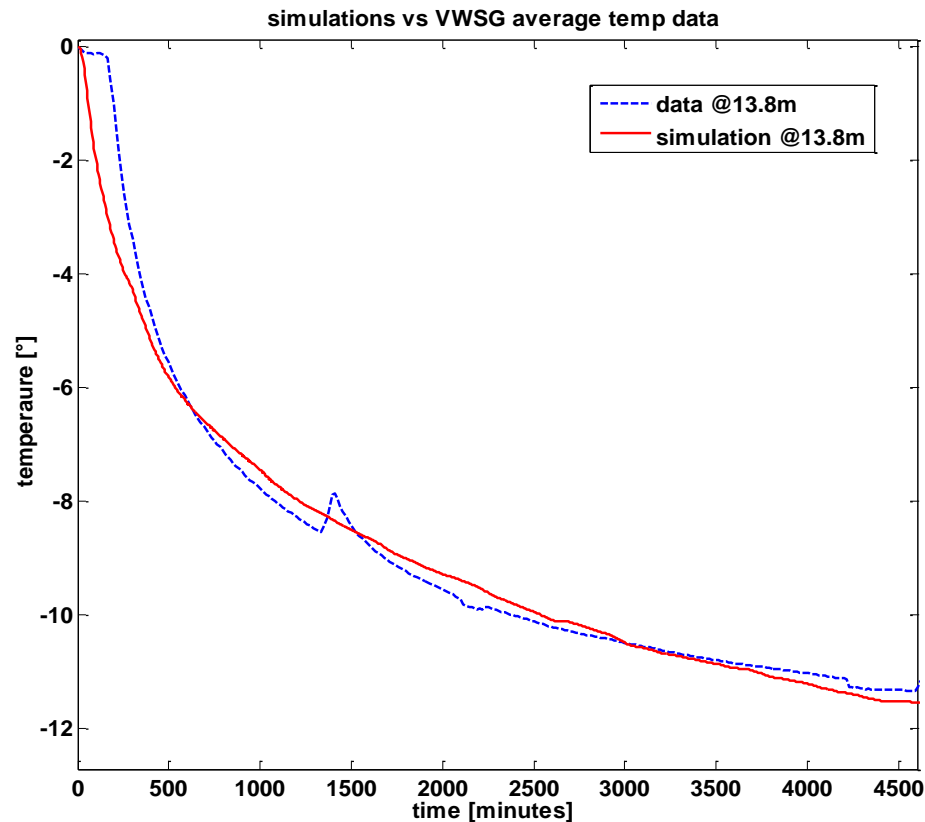
Numerical model validation against field data

- Simulation of outlet fluid temperature evolution compared to the measured one



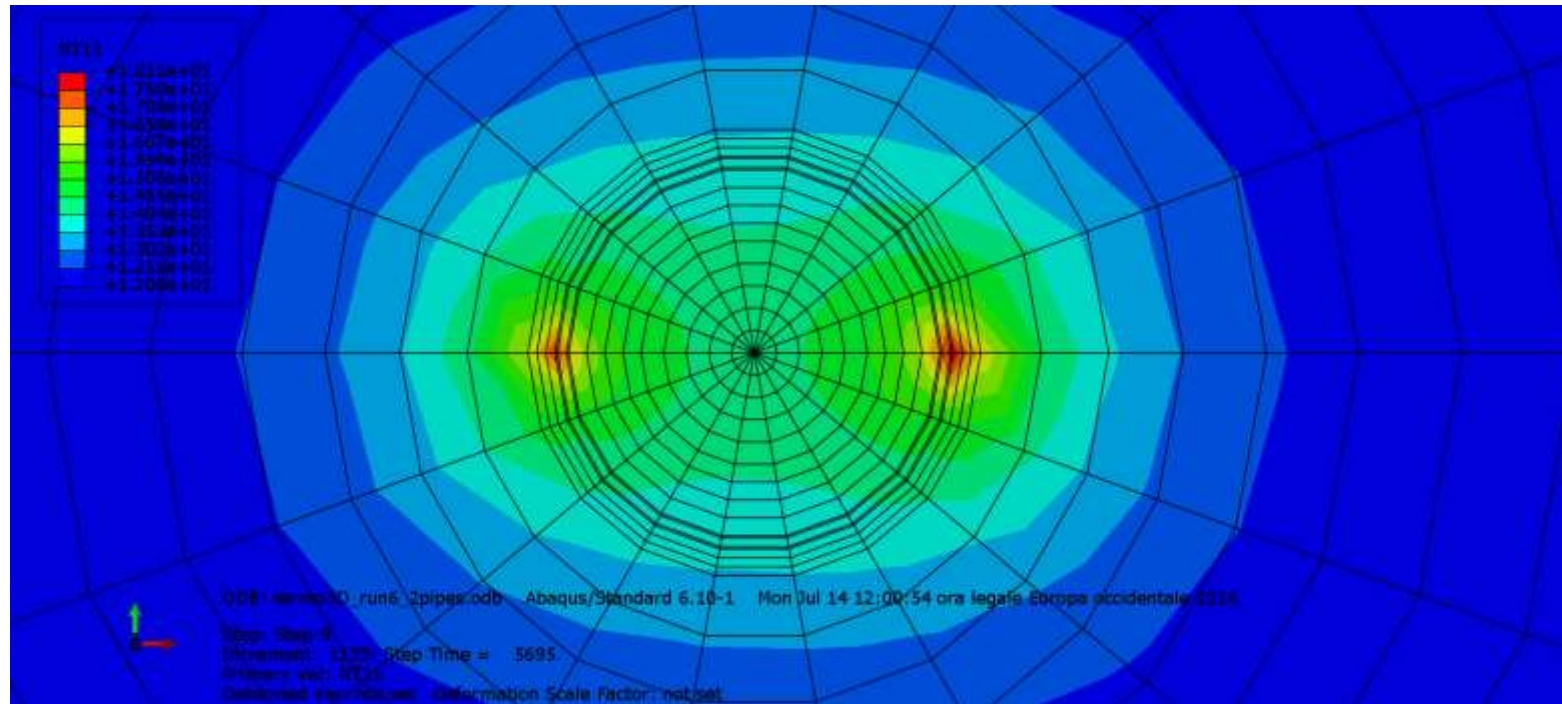
Numerical model validation against field data

- Simulation of concrete temperature evolution compared to the measured one



Example of simulation output

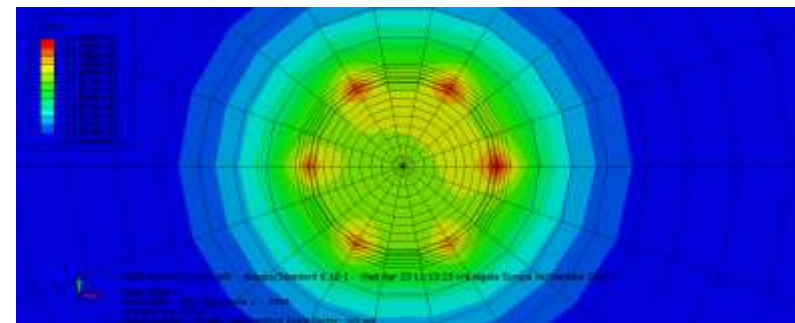
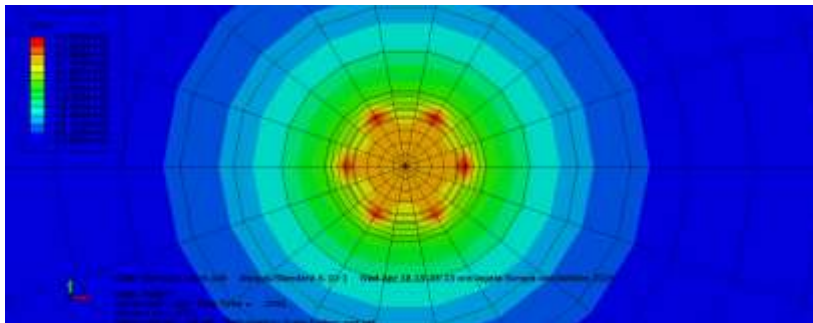
- Temperature contour lines evolution after 4 days of heat injection, cross-section view at pile mid-height



- Pile $\varnothing=1$ m, Single U-pipe

Design applications

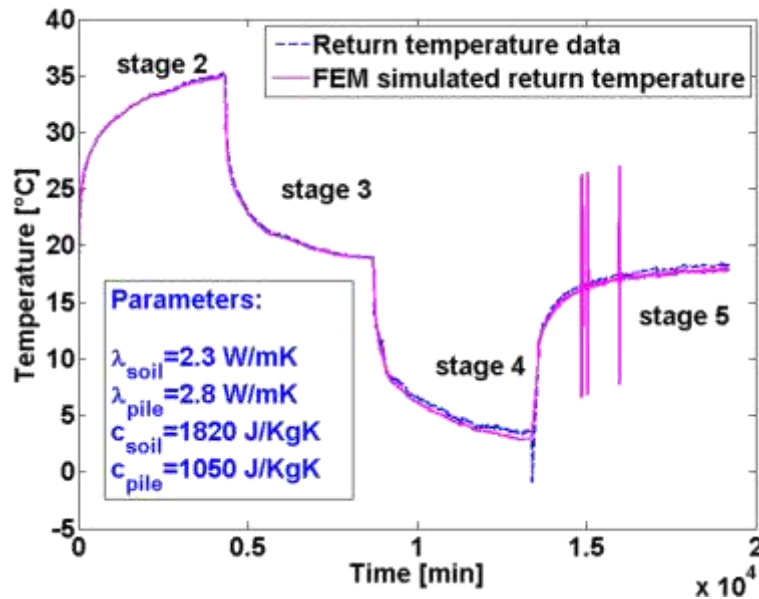
- Improved estimation of thermal properties during TRTs (back-calculating λ & c of soil & concrete by fitting measured T curves)
- Identification of the most important design parameters in enhancing energy efficiency, yet complying with geotechnical design
- Assessment of thermo-mechanical couplings that could interfere with the structural/geotechnical behaviour of the system (e.g. alteration of lateral bearing capacity)
- Application to other geothermal structures (e.g. tunnel linings, diaphragm walls...)



Example of design application/1:

Improved parameter estimation during TRTs

- Sensitivity analysis to identify best-fit values of thermal parameters for different TRT stages.



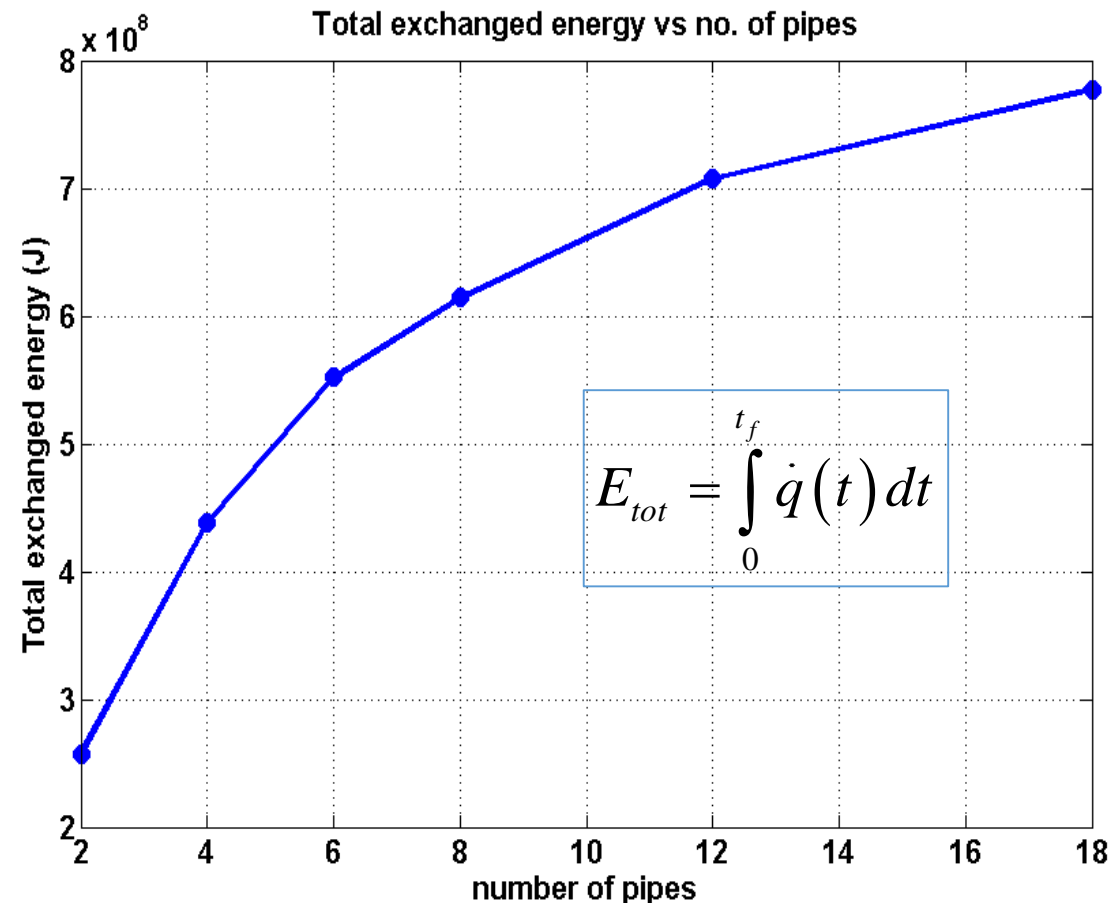
Simulation #	TRT stages	λ_c	λ_g	c_c	c_g	RMSE	Global RMSE
1	2&3	2.8	2.3	1050	1820	0.2308	0.659
	4&5	2.8	2.3	1050	1820	0.8653	
2	2&3	2.5	2.3	1050	1820	0.2826	0.670
	4&5	2.5	2.3	1050	1820	0.8686	
3	2&3	2.8	2.2	1000	2100	0.2312	0.652
	4&5	2.8	2.2	1000	2100	0.8557	
4	2&3	2.6	2.3	1050	2100	0.2532	0.669
	4&5	2.6	2.3	1050	2100	0.8750	
5	2&3	2.55	2.6	1000	2100	0.2917	0.666
	4&5	2.55	2.6	1000	2100	0.8635	

- More direct and accurate determination (compared to analytical and semi-empirical methods) of pile and ground physical properties λ_c , λ_g , c_c and c_g

Example of design application/2:

Energy efficiency vs no. of pipes installed

- Total exchanged energy after 4 days' heat injection simulation (initial $\Delta T = 8^\circ\text{C}$) for a 1m diameter pile

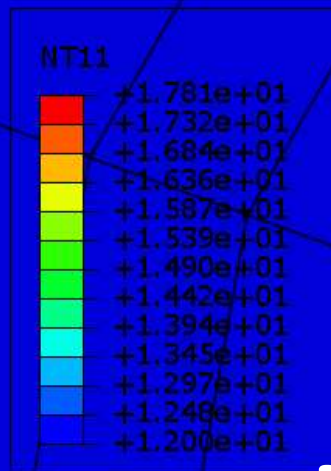


Conclusions

- An innovative 3D model to accurately reproduce the main features of heat transfer in geothermal systems was developed.
- Validation against field data shows the model's good prediction capabilities.
- The model can be used to gain further insight into thermal and thermo-mechanical aspects of geothermal systems, leading to improved design criteria.

References

- Cecinato, F., Loveridge, A. (2015). "Influences on the thermal efficiency of energy piles". *Energy* (82) : 1021-1033. [doi:10.1016/j.energy.2015.02.001]
- Loveridge, A., Cecinato, F. (2015). "Thermal performance of thermo-active CFA piles". *Environmental Geotechnics*. Accepted for publication.
- Cecinato, F., Loveridge, F., Gajo, A., Powrie, W. (2015). *A new modelling approach for piled and other ground heat exchanger applications*. XVI ECSMGE 2015, Edimburgh, UK [ISBN 072776067X]
- Loveridge, F., Cecinato, F. (2015). *What is the potential for pipe to pipe interactions in energy piles?* Proceedings of the International Symposium on Energy Geotechnics, Barcelona Spain, 2-4 June.



Thanks for your attention!

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Step: Step-9

Increment: 404; Step Time = 2020.

Primary Var: NT11

Deformed Var: not set Deformation Scale Factor: not set